

# Modeling and simulation of contact between rigid bodies

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## Navier-Stokes equations :

$$\begin{cases} \rho_f \frac{du}{dt} + \rho_f (u \cdot \nabla) u - \nabla \cdot \sigma = 0_{\mathbb{R}^d}, \Omega, \\ \nabla \cdot u = 0, \quad \Omega, \end{cases}$$

where  $\sigma$  the total stress tensor :

$$\sigma = -pI_d + \mu[\nabla u + (\nabla u)^T].$$

## Fluid definitions :

- $d = 2$  or  $d = 3$ , dimension.
- $\Omega \subseteq \mathbb{R}^d$ , fluid domain.
- $u : \Omega \rightarrow \mathbb{R}^d$ , velocity.
- $p : \Omega \rightarrow \mathbb{R}$ , pressure.
- $\mu \in \mathbb{R}^+$ , viscosity.
- $\rho_f \in \mathbb{R}^+$ , density.
- $I_d \in \mathbb{M}_{d,d}$ , identity tensor.

# Fluid model with moving rigid bodies

The bodies can translate and rotate with gravity, fluid forces acting on them and collision forces in body-body and body-wall interactions.

**Newton equations :**

$$m_i \frac{dU_i}{dt} = (m_i - \int_{B_i} \rho_f)g + F_i + F'_i,$$

$$\frac{d[RJ_i R^T \omega_i]}{dt} = T_i + T'_i,$$

***i*-th body definitions :**

- $B_i \subseteq \mathbb{R}^d$ , body domain.
- $m_i \in \mathbb{R}$ , mass.
- $J_i \in \mathbb{R}$  if  $d = 2$ , else  $J_i \in \mathbb{R}^d$ , moment of inertia.
- $R \in \mathbb{M}_{d,d}$ , rotation matrix.
- $U_i \in \mathbb{R}^d$ , translational velocity.
- $\omega_i \in \mathbb{R}$  if  $d = 2$ , else  $\omega_i \in \mathbb{R}^d$ , angular velocity.
- $x_i^{CM} \in \mathbb{R}^d$ , center of mass.

where  $g \in \mathbb{R}^d$  is the gravity vector,  $F'_i \in \mathbb{R}^d$ ,  $T'_i \in \mathbb{R}^d$  the collision forces and torque, and  $F_i \in \mathbb{R}^d$ ,  $T_i \in \mathbb{R}^d$  the hydrodynamic forces and torque acting on the body :

$$F_i = - \int_{\partial B_i} \sigma \cdot \vec{n} \quad \text{and} \quad T_i = - \int_{\partial B_i} \sigma \cdot \vec{n} \times (x_i - x_i^{CM}).$$

# Fluid model with moving rigid bodies

Coupling condition on the velocities on  $\partial B_i$  :

$$u = U_i + \omega_i \times (x - x_i^{CM}).$$

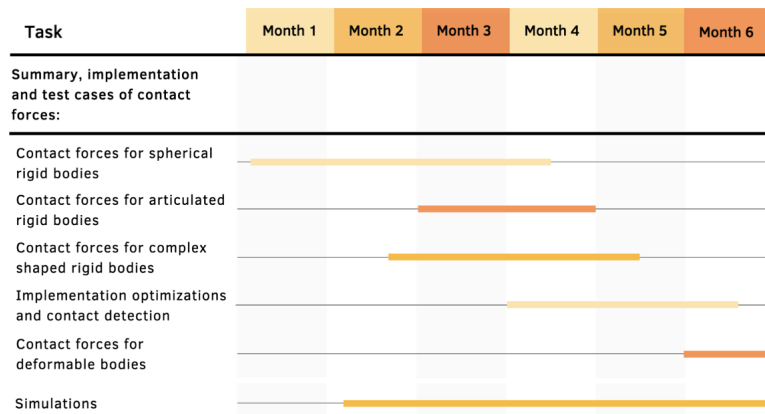
Fluid-body problem :

$$\left\{ \begin{array}{l} \rho_f \frac{du}{dt} + \rho_f (u \cdot \nabla) u - \nabla \cdot \sigma = 0_{\mathbb{R}^d}, \quad \text{in } \Omega, \\ \nabla \cdot u = 0, \quad \text{in } \Omega, \\ u = U_i + \omega_i \times (x - x_i^{CM}), \quad \text{on } \partial B_i, \\ m_i \frac{dU_i}{dt} = (m_i - \int_{B_i} \rho_f) g + F_i + F_i', \\ \frac{d[RJ_i R^T \omega_i]}{dt} = T_i + T_i'. \end{array} \right.$$



Decheng Wan, Stefan Turek. *Direct Numerical Simulation of Particulate Flow via Multigrid FEM Techniques and the Fictitious Boundary Method*, 2004.

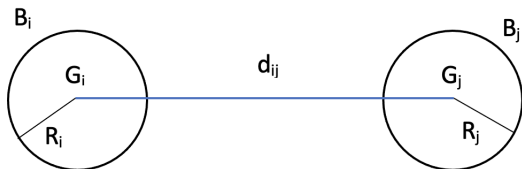
# Gantt chart



Full Gantt chart : <https://feelpp.github.io/swimmer/swimmer/latest/StageCeline/Introduction.html>.

# Collisions between spherical rigid bodies

**Smooth collision** : The velocities of the rigid bodies coincide at the points of contact.



We note  $d_{ij} = \|G_i - G_j\|_2$ , distance between the disk mass centers.

The repulsion force  $\vec{F}_{ij}$  has to verify three properties :

1.  $\vec{F}_{ij}$  is parallel to  $\overrightarrow{G_i G_j}$ .



R. Glowinski, T. W. Pan, T. I. Hesla, D. D. Joseph, and J. P eriaux. *A Fictitious Domain Approach to the Direct Numerical Simulation of Incompressible Viscous Flow past Moving Rigid Bodies : Application to Particulate Flow*, 2000.

# Collisions between spherical rigid bodies

- $|\vec{F}_{ij}| = 0$  if  $d_{ij} > R_i + R_j + \rho$ , where  $\rho$  the range of the repulsion force.
- For  $R_i + R_j \leq d_{ij} \leq R_i + R_j + \rho$  :

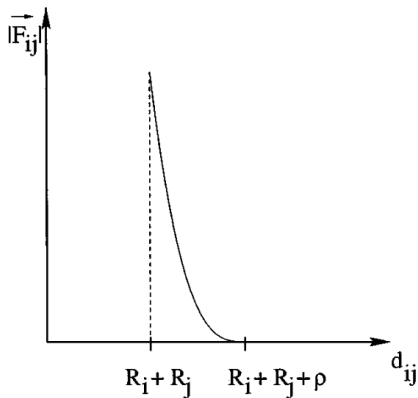


Figure – Repulsion force [1]

# Collisions between spherical rigid bodies

Definition of  $\vec{F}_{ij}$  for body-body interaction :

$$|\vec{F}_{ij}| = \begin{cases} 0, & \text{for } d_{ij} > R_i + R_j + \rho, \\ \frac{1}{\epsilon}(G_i - G_j)(R_i + R_j + \rho - d_{ij})^2, & \text{for } R_i + R_j \leq d_{ij} \leq R_i + R_j + \rho, \\ \frac{1}{\epsilon'}(G_i - G_j)(R_i + R_j - d_{ij}), & \text{for } d_{ij} < R_i + R_j. \end{cases}$$

where  $(R_i + R_j + \rho - d_{ij})^2$  a quadratic activation term and  $(G_i - G_j)$  gives the direction of the force.

The stiffness parameters are set to  $\epsilon \approx h^2$  and  $\epsilon' \approx h$ , if :

- $\rho \approx h$ ,  $h$  the mesh step.
- $\frac{\rho_b}{\rho_f} \approx 1$ ,  $\rho_b$  the body density and  $\rho_f$  the fluid density.
- The fluid is sufficiently viscous.



Decheng Wan, Stefan Turek. *Direct Numerical Simulation of Particulate Flow via Multigrid FEM Techniques and the Fictitious Boundary Method*, 2004.

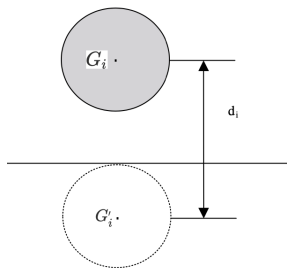


# Collisions between spherical rigid bodies

Definition of  $\vec{F}_i^W$  for body-wall interaction :

$$|\vec{F}_i^W| = \begin{cases} 0, & \text{for } d_i > 2R_i + \rho, \\ \frac{1}{\epsilon_W} (G_i - G'_i) (2R_i + \rho - d_i)^2, & \text{for } 2R_i \leq d_i \leq 2R_i + \rho, \\ \frac{1}{\epsilon'_W} (G_i - G'_i) (2R_i - d_i), & \text{for } d_i < 2R_i. \end{cases}$$

where  $\rho \approx h$ ,  $\epsilon_W = \frac{\epsilon}{2}$  and  $\epsilon'_W = \frac{\epsilon'}{2}$ .



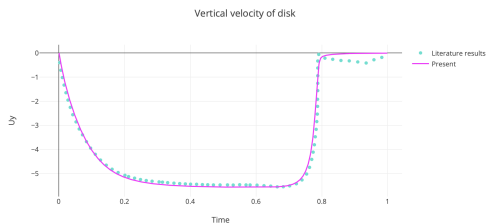
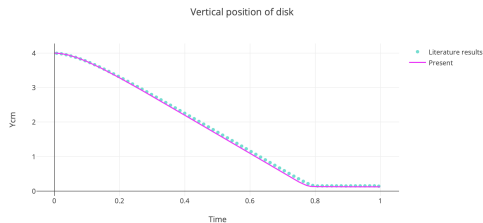
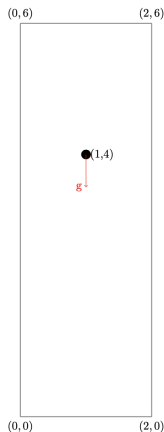
Total repulsion force applied on the body  $B_i$  :

$$|\vec{F}_i| = \sum_{j=1, j \neq i}^N |\vec{F}_{ij}| + |\vec{F}_i^W|,$$

where  $N$  the number of bodies.

Figure – Imaginary body [2]

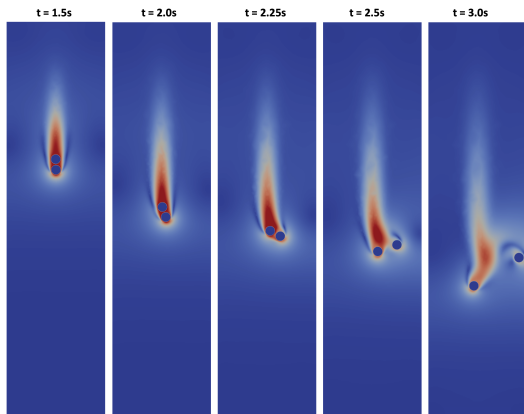
# Simulation : Disk-bottom interaction



The differences in vertical velocity can be explained by a higher repulsion force intensity used for the literature results [3].

# Simulation : Two disks interaction

## Drafting, kissing and tumbling phenomenon



K. Usman, K. Walayat, R. Mahmood, et al. *Analysis of solid particles falling down and interacting in a channel with sedimentation using fictitious boundary method*, 2018.



Decheng Wan, Stefan Turek. *Direct Numerical Simulation of Particulate Flow via Multigrid FEM Techniques and the Fictitious Boundary Method*, 2004.

# Collisions between complex shaped rigid bodies



## Narrow band fast marching method :

- Numerical technique for tracking the evolution of fronts propagating in direction normal to itself.
- The method computes the distance function  $D_i(X) : \mathbb{R}^d \rightarrow \mathbb{R}$  for each point of the mesh starting from a front  $\partial B_i$  :

$$\begin{cases} D_i(X) = d, & \text{where } d \text{ distance from } \partial B_i \text{ to point } X \in \mathbb{R}^d \\ D_i|_{\partial B_i} = 0. \end{cases}$$

- Narrow band :  $D_i(X)$  only computed in a near neighborhood of thickness  $d_{max}$  around  $\partial B_i$ .



J.A. Sethian. *A fast marching level set method for monotonically advancing fronts*,1996.

# Collisions between complex shaped rigid bodies

**Reformulation of  $\vec{F}_{ij}$  for body-body and  $\vec{F}_i^W$  for body-wall interaction :**

$$|\vec{F}_{ij}| = \begin{cases} 0, & \text{for } d_{ij} > \rho, \\ \frac{1}{\epsilon} (\arg \min_{X \in \partial B_i} D_j(X) - \arg \min_{X \in \partial B_j} D_i(X)) (\rho - d_{ij})^2, & \text{for } 0 \leq d_{ij} \leq \rho. \end{cases}$$

$$|\vec{F}_i^W| = \begin{cases} 0, & \text{for } d_i > \rho, \\ \frac{1}{\epsilon_W} (\arg \min_{X \in \partial B_i} D_\Omega(X) - \arg \min_{X \in \partial \Omega} D_i(X)) (\rho - d_i)^2, & \text{for } 0 \leq d_i \leq \rho. \end{cases}$$

**Angular momentum of  $\vec{F}_i = \vec{F}_{ij} + \vec{F}_i^W$  for body-body and body-wall interaction :**

$$\frac{d[RJ_i R^T \omega_i]}{dt} = T_i - \vec{G}x_r \times \vec{F}_i,$$

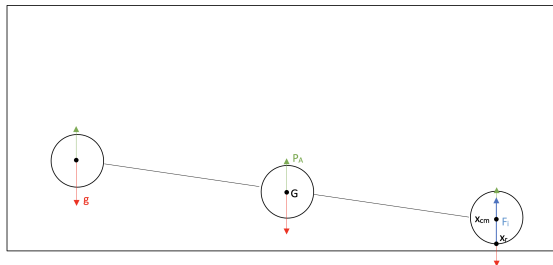
where  $G$  the mass center of the body and  $x_r$  the point where  $\vec{F}_i$  applies on the body  $B_i$ .



Tsorngh-Whay Pan, Roland Glowinski, Giovanni P.Galdi. *Direct simulation of the motion of a settling ellipsoid in Newtonian fluid*, 2001.

# Collisions between articulated rigid bodies

## Aligned three-sphere swimmer :



## Newton's equation describing the angular velocity :

$$\frac{d[RJ_i R^T \omega_i]}{dt} = T_i - \overrightarrow{Gx_r} \times \overrightarrow{F_i} + \overrightarrow{Gx_{cm}} \times (\overrightarrow{g} - \overrightarrow{P_A}),$$

where  $G$  the mass center of the swimmer,  $x_r$  the point where  $\overrightarrow{F_i}$  applies on the body,  $x_{cm}$  the mass center of one body,  $\overrightarrow{g}$  the gravity vector and  $\overrightarrow{P_A}$  the buoyancy.

# Conclusions of midterm internship

## **Regarding implementation and algorithms :**

Computational costs of the three algorithms were compared. The narrow band fast marching method proves to be efficient to determine the distance, nevertheless for 3D simulations optimizations will be necessary.

## **Regarding simulations and benchmarks :**

Various simulations have been performed to validate the models. Even if the results obtained do not always correspond exactly to the benchmarks, the same behavior is found.

## **Regarding other results :**

The implementation of the resolution of Stokes equations has been validated with benchmarks. The simulations performed with the three-sphere planar swimmer allow to conclude that its displacement will be the closest to the theoretical one when it is placed in a circular box of much larger size.

## **Simulation perspectives :**





- Multi-body simulations.
- Motion of a particle placed in an artery or zebra fish.
- Motion of a particle placed in fluids with imposed velocity.
- Motion of three-sphere swimmer near wall.
- 3D simulations.




## **Theoretical perspectives :**

- Considering literature on other approaches for contact force and detection.
- Considering simple cases of deformable bodies.



# References

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-  Tsorng-Whay Pan, Roland Glowinski, Giovanni P.Galdi. *Direct simulation of the motion of a settling ellipsoid in Newtonian fluid*, 2001.